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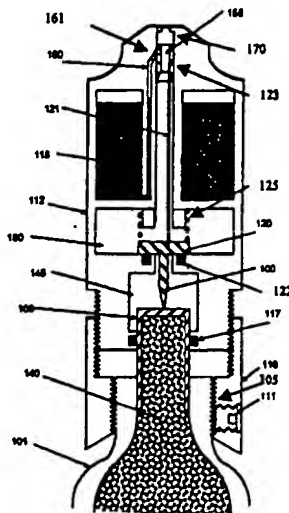
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(54) Title: METHOD AND APPARATUS FOR CO-APPLICATION OF GASES AND DRUGS TO POTENTIATE THEIR ACTION IN RELIEVING HEADACHES, ANGINA, AND OTHER AILMENTS



(57) Abstract: Apparatus and methods for co-application of physiologically active gas or vapor and drugs for the purpose of potentiating and/or controlling the effect of the drug and/or the physiologically active gas or vapor are provided, as well as apparatus allowing for improved flow control in gas dispensers. The methods include (i) simultaneous application of the gas and drug through inhalation or infusion and (ii) application of the drug and gas separately, with the drug applied by conventional means and the gas applied through inhalation or infusion of mucous membranes. Apparatus that include means for adjusting the particular mixture of gas and drug provided to the treated individual are described, as are apparatus that include a differential screw arrangement for controlling gas flow from a high pressure container.

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Like drugs, certain gases and vapors are physiologically active substances. The gases carbon dioxide and nitric oxide are known to be vasoactive, myoactive, and neuroactive [1]. Oxygen, nitrous oxide, helium, and dilute mixtures of nitric oxide may

5 also be vasoactive, myoactive, and/or neuroactive. In addition, vapors from certain substances that lower the pH of mucosa to a degree similar to that of carbon dioxide, such as hydrochloric acid (HCl), nitric acid (HNO₃), and hydrofluoric acid (HF) (all usually diluted with air) can be effective [6], and thus, in general, isocapnic mixtures of acid gases may be effective as well. Therefore, as used herein, "gas" and "gaseous" may refer
10 to any physiologically active gas or vapor.

If a drug is co-applied to a particular tissue or organ with CO₂, NO, or other vasoactive, myoactive, or neuroactive gas or vapor as taught and claimed herein, the speed and efficacy of the drug action in such tissue or organ may be controlled. As a specific example for CO₂, in an in vivo test, the ability of the drug atropine to inhibit
15 serotonin-induced bronchial smooth muscle contraction was found to be potentiated from 46% inhibition to 62% inhibition by co-application of a 10% CO₂ concentration [2]. Similarly, the inhibitory effect of the drug hexamethonium was potentiated from 37% inhibition to 67% inhibition by co-application of a 10% CO₂ [2].

The co-application of a drug with a gas or vapor can be performed in at least three
20 different ways: First, the drug and gas can be applied together locally by co-infusion and transmucosal co-absorption nasally, orally, and/or via the eye or ear. The form of the drug, of course, would need to be suitable for such infusion, for example, a fine powder or liquid. If the combination of the drug and gas is applied nasally or orally for local transmucosal absorption, the individual would substantially inhibit passage of the drug
25 and gas into his lungs and trachea by limiting inhalation of the gas and drug. Second, the drug and gas may be applied separately. The drug may be applied by any conventional means such as inhalation, pills, capsules, hypodermic injection or epidermal patches, and the individual may infuse a nostril or nostrils, mouth, eye or ear with the gas before, during or after application of the drug. As a variation of this method of co-application,
30 the gas may instead be inhaled. Third, a combination of the drug and gas may be inhaled.

As an example of the first method, a drug presently infused into the respiratory passages, mouth, eyes, or ears by entraining with air, e.g., as an aerosol, powder, or spray, can be applied instead by entraining with CO₂, e.g., through aspiration of a drug-containing liquid or powder by CO₂. In particular, the action of drugs developed and
35 presently used for relieving respiratory and headache symptoms may be improved by

5 their co-infusion with CO₂ or NO. The vasodilation induced by CO₂ or NO improves the speed and extent of absorption and distribution of the drug in the tissue in which it is co-absorbed with CO₂ or NO. This is beneficial through more rapid relief being obtained, and through reduction in the quantity of drug required to obtain the relief. Reduction in the required quantity of drug reduces the cost of treatment per dose and particularly
10 reduces the side effects of such drugs, which are severe restrictions to their present use.

With respect to the second method, a particular benefit of co-application of such drugs with CO₂ is that, in addition to the reduction of the total amount of drug required, the effect of the drug can be controlled or "modulated" in the course of its action after application. Inhalation or infusion of CO₂ prior to drug application can increase the
15 effectiveness and reduce the required quantity of the drug. Alternatively, inhalation or infusion of CO₂ after application of a drug can enhance the effect of the drug at a controlled rate; i.e., if a more rapid or more intense effect of the drug is desired, CO₂ can be inhaled or infused at the rate required to obtain the desired degree of enhancement. A particular advantage of such control is that the drug enhancement effect can be abruptly
20 terminated, by ceasing CO₂ inhalation or infusion, at the optimum level of beneficial drug effect that minimizes side or overdose effects. Also, since CO₂ is rapidly eliminated from the body via the bloodstream and respiration, the enhancement is reversible after CO₂ application is ceased, allowing continuous chronic adjustment of the drug effect.

An example of the beneficial regulation of the effect of a powerful drug by CO₂
25 inhalation or infusion is the co-application of CO₂ and nitroglycerin for the relief of acute angina and during onset of a heart attack (myocardial infarction). Nitroglycerin is a powerful vasodilator. Ordinarily persons suffering from angina or from symptoms of heart attack place a nitroglycerin tablet under their tongue (transmucosal delivery). If this is not adequate to relieve the symptoms within three minutes, another tablet is similarly
30 ingested. After another three minutes, if relief is not obtained, this process is again repeated. If the symptoms then persist, a person should be taken immediately to a hospital for emergency treatment. Some persons are extremely sensitive to the side effects of nitroglycerin however, including severe blood pressure reduction that can result in dizziness and fainting, especially after ingesting the second tablet, at a time when good
35 judgment and deliberate corrective action are required. A few minutes of delay can be

5 crucial after the onset of a heart attack. With co-application, CO₂ can be inhaled or infused after the first tablet to rapidly enhance and sustain its effects, possibly reducing the need for subsequent tablets. The effects of a second tablet of nitroglycerin can be initiated gradually and reversibly with CO₂ application to maintain and extend the optimum degree of pain relief without severe blood pressure reduction.

10 In all three methods cited only one physiologically active gas is used; however, physiologically active gases may be used together, with or without drugs. For example, CO₂ has been found to relax both central and peripheral airways in asthmatic adults [3]. Similarly, in both in vivo and clinical tests, inhaled low dose NO has been found to be as effective as sodium nitroprusside and prostacyclin in reducing transpulmonary gradient
15 and pulmonary vascular resistance, and is highly pulmonary vasoselective [6]. NO has also been found to reverse pulmonary hypertension [4,5]. Therefore, NO and CO₂ can be co-applied to potentiate their respective actions.

An essential aspect of co-application if control of drug effect is desired is that the CO₂, or similar physiologically active gaseous agent must be available for use by the
20 affected person immediately and conveniently at the time the symptoms appear. The hand-held portable dispenser described in U.S. Pat. Application No. 09/614,389 fulfills this requirement, but does not provide for a high flow rate which may be advantageous when co-application, and particularly inhalation, of a drug and gaseous agent are desired for potentiation. Additionally, the device described in U.S. Pat. Application No.
25 09/614,389 does not provide for simultaneously administering the gaseous agent and the drug.

It is therefore an object of the invention to provide a dispenser that allows a flow rate more suitable for co-application of a drug and gaseous physiologically active agent in certain circumstances. It is a further object of the invention to provide a dispenser
30 that allows for simultaneous co-application of a drug and gaseous physiologic agent and adjustment of the dose of the drug relative to the amount of gaseous agent administered. It is a further object of the invention to provide a method for controlling the effect of a drug through the co-application of a physiologically active agent in gaseous or vaporous form.

35

5 **Description of Background Art**

Inhalation devices, systems and methods for delivering carbon dioxide and other gases and aerosols to patients, with and without co-delivery of a drug are described in U.S. Patent Nos. 3,776,227; 3,513,843; 3,974,830; 4,137,914; 4,554,916; 5,262,180; 5,485,827; and 5,570,683. In general, the methods and devices that provide for co-
10 delivery of a drug and carbon dioxide or other gases do not do so for the purpose of potentiation. For example, carbon dioxide may be used simply as a safe propellant as shown in Wetterlin, U.S. Pat. No. 4,137,914. Additionally, in the devices shown, the gas and the drug are usually combined and stored together, which does not allow for adjustment of the amount of gas infused into the body. Such devices are therefore
15 inappropriate for the purpose of controlling the drug's effect by means of the gas.

Additional background art may be found in the following references:

- [1] Guyton AC, Hall JE. Textbook of Medical Physiology. Ninth Ed., W.B. Saunders Co., Philadelphia, 1996.
- [2] Tang A, Rayner M, Nadel J. "Effect of CO₂ on serotonin-induced contraction
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- [3] Qi S, Yang Z, He B. An experiment study of reversed pulmonary hypertension with inhaled nitric oxide on smoke inhalation injury. *Chung Hua Wai Ko Tsa Chih* 35(1):56-8, Jan 1997.
- [4] Loh E, Lankford EB, Polidori DJ, Doering-Lubit EB, Hanson CW, Acker
25 MA. Cardiovascular effects of inhaled nitric oxide in a canine model of cardiomyopathy. *Ann Thorac Surg* 67(5):1380-5, May 1999.
- [5] Pagano D, Townend JN, Horton R, Smith C, Clutton-Brock T, Bonser RS. A comparison of inhaled nitric oxide with intravenous vasodilators in the assessment of pulmonary haemodynamics prior to cardiac transplantation. *Eur J*
30 *Cardiothorac Surg* 10(12):1120-6, 1996.
- [6] Sterling G, et al. Effect of CO₂ and pH on bronchoconstriction caused by serotonin vs. acetylcholine. *J. of Appl. Physiology*, vol. 22, 1972.

Summary of the Invention

The current invention includes improvements and modifications to the dispenser
35 disclosed in U.S. Application No. 09/614,389 that permit the co-infusion of carbon

5 dioxide or similar physiologically active agents in the form of a gas or vapor, and a drug, resulting in the potentiation of the action of the drug and/or of the physiologically active agent. Dispensers and methods of application particularly suitable for such co-infusion and for inhalation are described. Alternative means for regulating and modifying the flow of gases in the previously described dispenser embodiments are also described
10 herein. Additionally, the present invention includes additional methods that allow for large volume inhalation of the dispensed gas.

Other features and advantages of the current invention will appear from the following description in which the preferred embodiments have been set forth in detail in conjunction with the accompanying drawings.

15

Brief Description of the Drawings

Figure 1 shows an embodiment of a co-infusion device before it is activated.

Figure 2 shows the embodiment of Fig. 1 after activation.

20

Figure 3 shows the embodiment of Fig. 1 when charged with high pressure gas.

Figure 4 shows the embodiment of Fig. 1 during discharge of the gas and drug solution.

25

Figure 5A shows the detail of device operation corresponding to Fig. 1.

Figure 5B shows the detail of device operation corresponding to Fig. 2.

30

Figure 5C shows the detail of device operation corresponding to Fig. 3.

Figure 5D shows the detail of device operation corresponding to Fig. 4.

Figure 6 shows the embodiment of Fig. 1 and illustrates the charge/dose and dose
35 rate adjustment features of the embodiment.

5

Figure 7 shows the detail of position selection for controlling the dose rate.

Figure 7A shows another view of the embodiment and shows certain details of the charge/dose features.

10

Figure 8 shows a second embodiment of a device which may be particularly appropriate for inhalation of the gas.

Figure 8A shows the detail of the flow rate adjustment and selection for the
15 second embodiment.

Figure 9 shows the embodiment of Figure 8 after perforation of the cap in a locked position.

20 Figure 10 shows the embodiment of Figure 8 in the activated position.

Figure 11 shows the embodiment of Figure 8 when dispensing gas.

25 Figures 12 A- E show application of gas to the nose, mouth, both nostrils, eye and ear using an embodiment of a gas dispenser.

Figure 13 shows an optional feature for dispensers which allows for dilution of the gas with ambient air.

30 Figure 14 shows an optional differential flow adjustment feature including the use of a ball detent particularly useful for low flow dispensers.

Figure 14A shows a cross-section detail of the embodiment of Figure 14A.

5 Figure 14B shows a variation of the device of Figure 14 including the use of an alternative detent.

Figure 14C shows a cross-section detail of the embodiment of Figure 14B.

10 Figure 15 shows flow rate adjustment and selection details for the embodiment of Figures 14A and 14C.

Figure 16A illustrates the analytical relationship between the critical needle taper angle α and the size of the annular orifice d for a needle displacement x .

15

Figure 16B is a detailed illustration of a standard needle configuration with exemplary dimensions.

Figure 16C is a detailed illustration of the preferred needle configuration with
20 exemplary dimensions.

Detailed Description of the Drawings

Dispenser Means For Co-Infusion Of CO₂ With Drug

25 Figs. 1-7 show a CO₂ dispenser embodiment that illustrates a means for the co-infusion of CO₂ with drugs. The dispenser embodiment in Figs. 1-7 is similar to the dispenser embodiments described for CO₂ infusion in U.S. Pat. Application No. 09/614,389. However, in addition to a container of pressurized gas or vapor, a flow regulator, and an outlet, the present invention further includes a container of a quantity of drug-containing liquid or powder agent and a means for mixing and releasing a controlled
30 dose of the drug agent and gas mixture through the outlet at a rate suitable for infusion into a body orifice such as the nose or mouth. Vertical motion in Figs. 1-5 and related figures is exaggerated to clarify the dispenser action.

The CO₂ cartridge 101 in the co-infusion embodiment shown in Figs. 1-7 has a threaded neck 105 and a cup-shaped sealing cap 106, both of which features have been
35 used in commercial gas cartridge embodiments separately but not necessarily together.

5 In the embodiments shown in Figs. 1-7 here a collar 110 is screwed onto the CO₂ cartridge neck 105. A set screw 111 in the collar 110 prevents movement of the collar 110 relative to the cartridge 101. A rotatable head 112 containing a seal-perforating needle 100, the drug agent 115, and the means for its controlled mixing and ejection with CO₂ is screwed into the fixed collar 110 and is sealed to the cartridge sealing cap 106 by
10 an O-ring gasket 117. As a safety feature the diameter of the sealing cap 106 above the location of the O-ring 117 should be less than the inside sealing diameter of the O-ring 117 so that any high pressure gas in the plenum 150 will be controllably released before the collar and head can be completely unscrewed and separated.

As shown in Fig. 1, the device is marketed with the sealing cap 106 intact. The
15 rotatable head 112 is screwed into the fixed collar 110 only partially such that the perforating needle 100 does not penetrate the sealing cap 106. The sequence of operation of the co-dispenser shown in Figs. 1-4 is shown in enlarged detail in Figs. 5a-5d.

To activate the device initially, the rotatable head 112 is screwed downward the full distance possible into the fixed collar 110, causing the needle 100 it contains to
20 penetrate the cap 106 that seals the cartridge 101 as shown in Figs. 2 and 5b. Thereafter, when the rotatable head 112 is unscrewed slightly the poppet valve 120 on which the needle 100 is mounted is closed and the needle 100 is lifted out of the orifice 130 it formed in the cap. As shown in Figs. 3 and 5c, this causes the chamber 145 between the cap 106 and the poppet valve 120 to become filled with high pressure CO₂ gas 140. The
25 volume of the gas dose chamber 145 is important since it defines the quantity of CO₂ gas 140, i.e., the gas dose that is mixed and co-infused with the drug.

The poppet valve 120 is biased shut against its O-ring-sealed seat 122 by a spring 125 that produces sufficient force to hold the poppet valve 120 shut against the force of the high pressure gas 140 on it. This force need not be large since the area of the orifice
30 130 sealed by the poppet valve 120 can be very small (a few mm²). When the rotatable head 112 then is screwed downward the needle 100 seats in and seals the orifice 130 in the cap 106 and the poppet valve 120 is lifted as shown in Figs. 4 and 5d, allowing the high pressure gas 140 in the gas dose chamber 145 to escape as a controlled burst into the gas plenum 150 which has a much larger volume, reducing the pressure ten-fold or more.
35 After the dose is administered, the pressure in the gas dose chamber would be about 1

5 atmosphere. From the gas plenum 150 the gas passes through the exit passage 126 and the venturi constriction of the passage. The poppet valve 120 is attached to a venturi control wire 121 that operates sleeve 123. Sleeve 123 is constructed to include a hole or gap 124. The gap 124 is positioned in the sleeve 123 and the sleeve is positioned within the venturi region so that when the poppet valve 120 is closed the gap 124 is not aligned
10 with the opening to the capillary passage 160. However, when the poppet valve 120 is opened as it is during the controlled burst, the venturi wire 121 lifts the sleeve 123 so that the gap 124 is aligned with the opening to the capillary passage 160. During the dose's passage through the venturi constriction, the controlled quantity of high velocity gas aspirates a correspondingly controlled amount of drug agent 115 through a capillary
15 passage 160 from the drug reservoir 115. The CO₂/drug mixture 199 then is discharged as a dose of spray through a hole in the top 171 of the dispenser. Subsequent doses are ejected by repeating the charge and discharge sequence represented by Figs. 3 and 4 or Figs. 5c and 5d respectively.

The actions required by the user to execute this sequence are illustrated in Figs. 6
20 and 7. To activate the device initially the user screws in the rotatable head 112 until it stops at the mark indicated as "Dose". The head is prevented from being unscrewed from its pre-activation position and is stopped at its fully screwed-in position by a sliding pin 180 in a slot 182 between the fixed collar 110 and the rotatable head 112. These limiting positions correspond respectively to the positions shown in Figs. 1 and 2 (and to Figs. 5a
25 and 5b) and are labeled "a" and "b" respectively in the schematic drawing of the pin 180 and slot 182 shown in Fig. 7. To deliver doses, the user first rotates the head against a torque-producing spring 655, which includes a section 654 that is engaged with the pin 180, to the charging position "c" in Fig. 7 corresponding to Figs. 3 and 5c, where the head 112 becomes locked by the pin 180, now held in a retaining well 653. The user then
30 applies the top of the dispenser 608 to his nose or mouth and pushes a button 600 which releases the sliding pin 180 from its retaining well 653. The head 112 then rotates rapidly back to position "d" (corresponding to Figs. 4 and 5d) under the action of the spring, completing the dose-delivering sequence of processes described in the preceding paragraph. As shown in Fig. 6, subsequent doses are delivered simply by "cocking" the
35 device by rotation as shown by arrow 602 and pushing a button 600 to deliver the dose by

5 an automatic counter-rotation. Note that left-handed screw threads are used in the embodiment shown, although a standard right-handed thread may also be employed. Accordingly, it is not necessary for the user to observe the position of the head relative to the collar 110 since the action involves rotation from the limiting position a in one direction to the limiting position d in the opposite direction. It will be clear to those of
10 ordinary skill in the art that this same type of automatic action can be obtained also by combining a rotary cocking action with a triggered linear return between the charging and dose positions such as is found in the action of retractable ball-point pens.

For a device designed to dispense a particular drug, the volume of CO₂ gas in a dose, the quantity of drug that it aspirates and the rate of infusion of the mixture has to be
15 chosen carefully. Obviously, the quantity of drug in a dose should be that determined in clinical trials and selected to be the most effective under a given set of circumstances, taking into account the enhanced effect of the drug caused by the co-application of CO₂. However, the quantity of CO₂ accompanying each drug dose may not necessarily be that determined in clinical trials to obtain the optimum potentiation, since both the quantity
20 and concentration of CO₂ infused and the rate of its infusion must be acceptable to the user.

The relative quantities of drug and CO₂ in the dispensed mixture are determined by the relative diameters of the capillary opening 161 and the venturi throat 155. The rate of discharge of the mixture is limited by the series flow impedance from the dose
25 chamber 145 through the poppet valve 120, plenum 150, and venturi 155. Generally, the tolerable steady flow rate of gaseous CO₂ into the nose is in the range 2-10 cc/sec for at least 2 seconds corresponding to the approximate volume of the nasal and sinus passages. However, patients may develop a short-term tolerance after continuous use or successive uses that allows for a higher flow rate. In addition, the inventors have access to new
30 experimental evidence that suggests that under certain circumstances much higher initial flow rates, on the order of 1 to 2 liters/minute may not only be tolerated, but be beneficial, in relief of certain symptoms. The tolerable CO₂ infusion rate is more than 10 cc/sec for an indefinitely long period into the mouth. However, although other designs may be appropriate in specific circumstances, in a dispenser for general adult use that
35 includes nasal infusion, the gas dose chamber 145 at minimum can contain an amount of

5 gas corresponding to 4-20 cc at room temperature and atmospheric pressure. If the CO₂ pressure in the cartridge 101 and in the dose chamber 145 is nominally about 60 atmospheres (which is achievable by known cartridge designs -- although such cartridges are not necessarily currently marketed for medical use), the volume of the dose chamber 145 should be in the range 0.07-0.33 cc, equivalent to a cubic chamber with 4-7 mm edge
10 length. The diameter and height of the gas dose chamber 145 therefore need to be only slightly larger than the typical 3 1/2 mm sealing cup diameter of currently available cartridges. A different size gas dose chamber would, of course, be required given different pressure, desired volume of gas, or other changes in the assumptions described. The concentration of the drug solution and the relative sizes of the venturi 155 and
15 capillary openings 161 are chosen for the expulsion of this quantity of CO₂ to aspirate the clinically appropriate drug dose (typically 10-60 mg for many drugs), although trials may show that some individuals prefer more than one application of CO₂ to obtain a full drug dose.

Because the desirable flow rate of gaseous CO₂ has been found to be highly user-
20 subjective, it is preferable to have a means for the user to select the dose speed, i.e., the period over which the gas and drug dose is delivered as a pulse. After the device is activated as is shown in Fig. 2 and 5b, the dose speed can be modified conveniently and simply in the illustrative embodiment by loosening the set-screw 111 that prevents collar rotation, unscrewing the collar 110 to the desired, marked positions 609 as shown in Fig.
25 6, and re-tightening the set-screw 111. The fastest dose delivery is obtained in the post-activation position (Figs. 2 and 5b) since the poppet valve 120 is opened fully in that position, but if the collar 110 is unscrewed, the poppet valve 120 is adjusted so that it is only very slightly open when the head is at position "d". That position would correspond to the minimum flow rate required for aspiration of the proper quantity of drug. The
30 range of adjustment between the positions of the collar 110 giving maximum and minimum permissible flow rates, shown as "F" and "S" in Fig. 6, is limited by the width of the slot 182 in the threaded cartridge neck 105 in which the set-screw 111 is seated.

It is anticipated that additional features may need to be included to make the various chambers and passages easily manufacturable, and other aspects not shown could
35 be incorporated in the design of a commercial product.

5

Dispenser Means For Co-Application Of CO₂ And Drugs By Inhalation and Infusion

The embodiment of the invention described above is a means for co-infusion or co-inhalation of a CO₂ /drug mixture as a measured dose into the nasal and respiratory passages. That device and the devices described in U.S. Application No. 09/614,389 are not generally suitable for inhalation of CO₂ into the lungs to potentiate the effect of drugs applied by other means. During inhalation the CO₂ is mixed with inspired air; therefore, a flow rate and quantity of CO₂ much greater than that achievable with the dispenser embodiments previously described is necessary. The required flow rate for co-application of drugs and of CO₂ by inhalation, and the means for achieving the required flow rate in a portable device are now described.

In general, depending on the size and other attributes of the individual, 1 to 2 liters of air inspired over a period of 1 to 2 seconds is comfortable for most adults. This corresponds to a flow rate range of 1 to 4 liters/second of air. The concentration of CO₂ in expired breath is about 6%. Most experimental research with inhalation of CO₂ by humans and animals has employed maximum concentrations of approximately 10%-70% CO₂ in air. However, above 10% concentration the individual may suffer a feeling of suffocation, and above 30% continued inhalation will result in the individual losing consciousness. If a 10% concentration of CO₂ is desired, a dispenser that provides a controlled flow rate in the range 100-400 cc/sec is needed. This is more than an order of magnitude greater than the typical maximum tolerable initial flow rate for infusion of 100% CO₂ into the respiratory passages for which the previously described embodiments are suitable.

Figs. 8-11 show a dispenser embodiment for controllably delivering CO₂ at an adjustable rate in the 100-400 cc/sec range suitable for co-application of CO₂ with drugs by inhalation or for treatment of asthma and other conditions by inhalation of CO₂ alone. The dispenser embodiment in Figs. 8-11 is similar to that described for CO₂ infusion in U.S. Application No. 09/614,389 in that it is a hand-held portable dispenser consisting of a pressurized cylinder of CO₂ screwed into a dispenser head assembly. The CO₂ cartridge 801 in this embodiment has a threaded neck 805 and a plug-type sealing cap 806 and is screwed into a dispenser head with a seal-perforating needle 800 similar to

5 that described in U.S. Application No. 09/614,389. In the device as marketed to the user, the cartridge 801 is screwed into the head 812 until the tip of the needle 800 just touches the top of the intact sealing cap 806 (i.e. without penetrating it) as shown in Fig. 8. The user activates the device by screwing the cartridge 801 onto the needle-bearing head 812 as indicated by arrow 816, thus perforating the sealing cap 806. The user may select the
10 rate at which the device can deliver CO₂ gas by choosing the distance that the needle 800 penetrates the cap 806, and thereby the size of the orifice 830 produced in the cap. The device would be activated by unscrewing the head and depressing the lever to release the gas. The degree of rotation required to produce each selectable rate may be indicated by number or other indicator markings on the dispenser head as shown in Fig. 8a.

15 However, while it is possible to select the flow rate by screwing the cartridge 801 only part way onto the head 812 to achieve the degree of seal perforation by the needle 800 required to obtain that rate, it is preferable to screw the cartridge 801 and head 812 together as far as possible, making the maximum possible orifice in the sealing cap 806. In this position, which is shown in Fig. 9, gas cannot be released from the cartridge
20 801 since the needle 800 is locked in its fully seated position. The user can select this position, therefore, to carry the device without risk of unintentional release of CO₂ gas. Since both the pressure in the cartridge and the orifice size are known, the maximum flow rate is also known. As shown in Fig. 8A, in this preferred embodiment, the device is activated for use by partially unscrewing the head 812 as is indicated by arrow 817, shown in Fig. 10, until the arrow 802 on the cartridge 801 is opposite the marking 831 on
25 the head 812 that indicates the flow rate that the user desires. This flow rate is essentially a portion of the known maximum flow rate permitted by the size of the orifice, and the markings may be an arrow 802 on the cartridge and numbers 831 on the head that represent either a percentage of the maximum flow or the number of cc/sec.

30 Upon activation, the head 812 and cartridge 801 are in the position shown in Fig. 10. In the present embodiment the needle 800 is held firmly seated in the cap orifice 830 by the force of a spring 829 acting on a sliding needle mount 834 as shown in Fig. 10, thus preventing flow of gas from the cartridge 801. In the present embodiment gas 866 can be controllably released up to the desired flow rate by depressing the dispensing
35 lever 815 as shown in Fig. 11. The lever 815 lifts the sliding needle mount 834 and

5 thereby unseats the needle 800 to open, directly and variably without rotating the head
812, the orifice 830 in the cartridge 801 seal to obtain the desired high flow rate. A
compressible (sponge-type) gasket ring 852 seals the dispenser lever penetration and
threads to prevent excessive gas leakage from the low pressure gas region. When the
lever 815 is released, the spring 829 returns the needle mount 834 and needle 800 to the
10 fully seated position as in Fig. 10, terminating the gas flow 866 from the openings in the
top of the head 871. To repeat the flow, the user again presses and releases the
dispensing lever 815. After the dispensing process is completed, the user can screw the
head back to the locked position shown in Fig. 9 for secure transport in a pocket or purse.

 The direct lever-actuated motion of the needle sliding mount 834 permits the
15 greater linear motion of the needle 800 out of the orifice 830 that is required to obtain a
high flow rate. Therefore, provided that the orifice 830 is large enough, using this
device, the user can selectively obtain the higher flow rates needed for inhalation of CO₂.
The controllability and simplicity of the needle-in-cap flow rate selection and adjustment,
employed in previously described embodiments, is retained without the requirement of a
20 large or coarse rotation of the head to a high flow position.

 It is also possible to potentiate drug action solely by mucosal infusion. While
generally, infusion is best performed using an initial lower flow rate, on the order of .5
cc/second to 20 cc/second depending on the tolerance of the particular individual, certain
applications allow and may even require a high initial flow rate. The lever activated
25 embodiment may be modified to provide a low flow rate, but the rotably activated
embodiments described in U.S. Application No. 09/614,389 are also suitable, and indeed
any low flow source of gas could be used. The general method of application is as
follows: the selected drug is applied by any standard method including but not limited to
inhalation, pills, capsules, injection, or epidural patch. As shown in Fig. 12A-B, the
30 individual P then infuses oral and nasal mucous membranes by placing the source of low
flow rate CO₂ or other appropriately physiologically active gas or vapor in or around a
facial orifice, such as the mouth or nostril, while substantially inhibiting the flow of the
CO₂ into the trachea and lungs by limiting inhalation of the CO₂. If the mouth is infused
the gas is allowed to exit from the nostrils. Alternatively, one or both nostrils may be
35 infused either by using the dispenser head shown in Fig. 12B or by use of a cup or similar

5 device that covers both nostrils as shown in Fig. 12E. The gas is allowed to flow from a remaining open orifice, i.e., either the mouth, the uninfused nostril, or both as appropriate. Completely holding the breath is not necessary to substantially prevent inhalation of the CO₂. With practice, it is possible for the individual to breathe through an uninfused orifice: for example, if one nostril is infused and the gas is allowed to exit
10 though the other nostril, it is possible for the individual to breathe through the mouth without substantial inhalation of the infused gas. The eye or eyes may also be infused using a cup as shown in Fig. 12C or merely by holding a hand over the eye and releasing the gas between the hand and the eye. Persons of ordinary skill in the art will appreciate that a double cup could be developed to infuse both eyes simultaneously, and similarly
15 appropriate heads could be developed to infuse the mouth and one nostril. The ear or ears may also be infused as shown in Fig. 12D. Note that a similar process may be used with the first embodiment to infuse a mixture of a drug and gas into various facial orifices.

Infusion can be continued to the limit of tolerance or until the desired potentiation effect is realized. Since most individuals develop a temporary increased tolerance after
20 extended applications or repeated applications, it may be possible and desirable to increase the duration of additional infusions after a few applications when all applications occur within a short time of each other, i.e., approximately 1 to 20 minutes between each application.

25 Optional Features

Depending upon the particular market for and/or intended use of the particular dispenser, some or all of the additional features may be added to the embodiments described above, and may also be incorporated into the embodiments described in U.S. Application No. 09/614,389.

30

Dilution Of CO₂ With Air

As shown in Fig. 13, a venturi 1303 region can be added to the dispenser head 1312 that allows a quantity of ambient air to be mixed with the CO₂ dispensed. The high pressure CO₂ 1350 flows past the needle 1300 and becomes low pressure CO₂ 1351. The
35 low pressure CO₂ moves past the air inlet 1333 and mixes with ambient air. The

5 concentration of CO₂ in the dispensed gas 1352 will thus be lower than 100% to the degree that air is admitted into the air inlet 1333. This will, in part, be a function of the size of the air inlet 1333. Additionally, the user can place his finger wholly or partially over the inlet 1333 to adjust the CO₂ concentration to that which is optimum for him at a given time, e.g., at a given stage of nasal inflammation or other mechanical partial
10 blocking means may be used with the same effect. This dilution feature also extends the duration of application obtainable from the dispenser for a fixed quantity of CO₂.

Differential Flow Adjustment

With reference to Fig. 14, in the initial embodiments described in U.S.
15 Application No. 09/614,389, the flow of CO₂ is adjusted by screwing the cartridge neck into and out of the dispenser head, thereby moving the needle into and out of the orifice in the cartridge seal. Although this is an extremely simple and practicable means for flow adjustment, it requires an extremely fine thread on the cartridge neck especially for the conventional needle size and shape described in Fig. 4A of U.S. Application No.
20 09/614,389. This can be understood by considering that the axial movement of the needle required to obtain the required 2-10 cc typical flow rate is in the vicinity of 1-2 thousandths of an inch (mils). For the standard threaded cartridge using 24 threads per inch, this means that the full range of flow rate adjustment is obtained with rotation of the head less than 1/20th of a turn (less than 20°). As described in U.S. Application No.
25 09/614,389, the required rotation for convenient control of the typical maximum flow rate is in the range of 30° to 120°, with the optimum being near but less than 120° rotation. This means that a very fine thread on the cartridge neck 1405, more than 100 threads per inch, is required to approach the optimum degree of flow rate control by the means described in U.S. Application No. 09/614,389.

30 While the production of such very fine threads is possible in principle, their production in a mass-produced low-cost device may be impractical for several reasons. First, machining such fine high-precision threads is substantially more expensive than machining standard threads on cartridge necks, and such threads would be expensive to produce on a molded plastic head. Second, cartridge threads now are generally protected
35 from corrosion by applying a coating that would fill and clog fine threads. Third, it is

5 impractical to hand-assemble items with such very fine threads because highly precise alignment is required to avoid cross-threading, resulting in a need for an expensive high-precision assembly machine.

Figs. 14 and 14A illustrate an embodiment of a low flow dispenser incorporating a differential screw threads that allow the user to obtain the required degree of rotational
10 control with relatively coarse and easily produced threads. A three-part assembly consisting of a head 1412, a sleeve 1440 and a collar 1410 is used. The head 1412 is similar to the dispenser heads in other embodiments, including those in U.S. Application No. 09/614,389 in that it incorporates a perforating and flow-regulating needle 1400 along with ports in the top of the head 1413 for delivering the high pressure gas 1495 in
15 the container as the low pressure dispensed gas 1414. The collar 1410 is screwed onto the CO₂ cartridge neck 1405 and selectively fixed there against rotation, e.g. by a set screw (not shown) as in the co-infusion embodiment in Figs. 1-4. The head 1412 also is fixed against rotation by tabs 1417 that extend from the head 1412 into slots 1418 in the collar 1410, permitting axial relative motion between the head 1412 and collar 1410 but
20 not rotational relative motion between them. A spring or gasket 1493 is situated between the head 1412 and collar 1410. The sleeve 1440 is threaded over both the head 1412 and collar 1410, bridging the space between them and thereby determining their relative axial positions.

The meshing threads 1490 between the collar 1410 and the sleeve 1440 are
25 slightly coarser than those 1491 between the head 1412 and the sleeve 1440. Thus, as the sleeve 1440 is rotated relative to the head 1412 and collar 1410, the distance between the head 1412 and the collar/cartridge assembly is changed. For example, if there are 24 threads/inch in the collar end of the sleeve and 26 threads/inch in its head end, a single turn of the sleeve relative to the head and collar/cartridge assembly advances the
30 collar/cartridge assembly into the sleeve by 1/24 inch but withdraws the head from the sleeve by only 1/26 inch; therefore, the distance between the head and collar/cartridge assembly is decreased by $1/24 - 1/26 = 2/624 = 0.0032$ inch ≈ 3.2 mils, which also is the distance that the needle 1400 is advanced into the cartridge 1401 by a 360° turn of the sleeve. It can be seen that the required ~1-mil motion of the needle 1400 into and out of
35 the cartridge orifice 1430 may be obtained with the near-optimum 120° rotation of the

5 sleeve using easily produced coarse threads. Another advantage of the configuration in this embodiment is that a detent ball 1426 and slot 1428 arrangement 1425, including a limiting slot 1496 can be incorporated easily into the head/sleeve assembly as shown in Fig. 14 without requiring the cartridge manufacturer to produce a special slotted thread in the cartridge neck. With specific reference to Figures 14B-C, as an alternative, other
10 detent arrangements, such as a pawl 1497, could also be used, and persons of ordinary skill in the art will appreciate that other alternatives are also available.

Fig. 15 illustrates the flow rate adjustment and selection features that may be incorporated into the embodiment of Fig. 14. The collar 1410 is fully screwed into the sleeve 1440 so that the collar arrow 1454 is at the position indicated as "0" 1453 on the
15 sleeve 1440, and the cartridge 1401 is screwed into the collar 1410 until the tip of the needle 1400 just touches the top of the intact sealing cap 1406 (i.e. without penetrating it). The user activates the device by screwing the cartridge 1401 into the collar until the arrow 1451 on the cartridge 1401 is opposite the number on the collar 1452 that indicates the maximum flow rate that the user desires, which corresponds to the degree of seal
20 perforation by the needle 1400 required to obtain that maximum rate. Thereafter, by rotating the sleeve 1440 the user can select the desired portion of that maximum flow delivered (which may be expressed by sleeve indicator number marks 1453 as a percent of the maximum flow) by rotating the sleeve 1440, to the corresponding sleeve indicator number 1453 position opposite the collar arrow 1454 or by counting the number of detent
25 "clicks" corresponding to that position.

Preferred Needle Configuration

As described in U.S. Application No. 09/614,389 the preferred needle configuration allows the desired very small change in the orifice area to be effected by
30 relatively large axial displacement of the needle.

While such modification is of primary advantage when used in conjunction with the embodiments shown in U.S. Application No. 09/614,389, this modification may also have advantages in the lever embodiment shown herein or in any embodiment in which it is desirable that a large displacement of the needle produce only small change in the flow.

5 An appropriate needle configuration is shown in Fig. 16C. The lowermost point of the needle 1603, over a distance approximately equal to the thickness of the cartridge seal, has essentially the same shape and size as the puncture point shown in Figure 4A of U.S. Application No. 09/614,389 and shown here in Figure 16B. The configuration of this point is an optimum compromise between the strength of a blunt point and the
10 reduced force requirement of a sharp point in the puncture process. However, the needle region 1602 above the point which is adjacent to the orifice formed in the cap, determines the size of the annular flow-controlling orifice when the needle is partially withdrawn. Thus, the modification of the configuration of this region of the needle may be used to obtain the required flow regulation characteristics of the dispenser.

15 As shown in Fig. 16A, the axial needle displacement giving a required size of the flow-controlling annular orifice is inversely dependent on the taper angle of the needle in the seat region 1602. This taper angle is approximately 20 degrees in the initial needle configuration shown in Fig. 16B, which required a displacement x of about 0.001 inch between zero flow and full flow as obtained by a 10 degree rotation of the head with 28
20 threads/inch. Therefore, to obtain the 120 degree optimal head rotation, the needle seat taper angle α must be about 1.7 degrees for 28 threads/inch or about 3 degrees as indicated by α_2 for the preferred 48 threads/inch.

 While preferred embodiments of the present invention are described above and in the following claims, it is contemplated that various modifications may be made without
25 departing from the spirit and scope of the invention. For example, while CO₂ has been particularly described, other gaseous and vaporous vasodilators including NO and dilute acid vapors, as well as other physiologically active, gaseous substances (e.g., vasoactive, neuroactive, myoactive, etc.), have similar potentiating effects and are intended to be included as possible choices for substances to be co-applied with a drug for the purpose
30 of increasing and/or controlling the effect of the drug. Furthermore, many of the features of the various embodiments described herein can be combined or added to other devices to obtain the optimum combination of features for particular applications and markets.

CLAIMS

What is claimed is:

- 5 1. A device for generating a flow of a mixture of a selected drug and a gaseous potentiating substance for administration to an individual comprising:
- a container for pressurized holding of the gaseous potentiating substance, defining an opening sealed with a cap;
- a head adapted for attachment to the container, said head defining a chamber
- 10 wherein when the head is attached to the container the opening is within the chamber and wherein the opening and cap are axially translatable to various positions within the chamber, a plenum, an exit passage and at least one outlet, wherein the plenum is connected to the outlet by means of the exit passage, said exit passage forming a venturi region near the outlet, and wherein the chamber selectively communicates with the
- 15 plenum by means of a valve, said valve biased to a closed position; said head further comprising a reservoir adapted for holding an aspiratable agent that contains the drug and a capillary passage connecting the reservoir and the venturi region of the exit passage; and said head further including a dispensing region near the outlet adapted for applying a discharge from the outlet to a facial orifice of the individual; and
- 20 a needle adapted for perforating the cap, said needle attached to the valve and positioned such that the needle perforates the cap when the opening and cap are in a first preselected position within the chamber and forms an orifice of a desired size; and such that when the opening and cap are in the first preselected position, the needle seals the orifice and the valve is forced open;
- 25 a lock for holding the opening and cap in a second preselected position within the chamber wherein the needle is at least partially removed from the orifice and the valve is closed, whereby the chamber is filled with the gaseous potentiating substance at a high pressure;
- 30 a first spring for moving the opening and cap relative to the chamber to the first preselected position when the lock is released, whereby the gaseous potentiating substance moves from the chamber to the outlet, passing through the plenum and the

5 venturi region of the exit passage, and aspirating a selected amount of the agent,
discharging a mixture of the agent and the gaseous potentiating substance at the outlet.

2. The device of claim 1 wherein the dispensing region is adapted to apply
the discharge to a nostril of the individual.

10

3. The device of claim 1 wherein the dispensing region is adapted to apply
the discharge to the individual's mouth.

4. The device of claim 1 further comprising:

15 a collar adapted to be fixedly attached to the container, wherein the head is
simultaneously attachable to the container and the collar.

5. The device of claim 4 wherein the container defines a region near the
opening and cap that is substantially cylindrical and that defines a first set of screw
20 threads, the collar defines a substantially cylindrical aperture that further defines a second
set of screw threads adapted to mate with the first set of screw threads and also defines a
third set of screw threads; and the head defines a fourth set of screw threads adapted to
mate with the third set of screw threads, and further includes a gasket adapted to seal the
head to the container.

25

6. The device of claim 1 wherein the first preselected position may be
selected and modified by the user.

7. The device of claim 5 wherein the first preselected position may be
30 selected and modified by the user.

8. The device of claim 7 wherein the first preselected position may be
modified by rotably adjusting the collar to the selected location along the central axis of
the container such that the valve is open to a desired amount when the opening and cap

5 are in the preselected first position relative to the head and wherein the collar further includes a set screw adapted for holding the collar at the selected location.

9. The device of claim 7 wherein the collar further includes markings corresponding to a range of possible first preselected positions.

10

10. The device of claim 8 wherein the collar further includes markings corresponding to a range of possible first preselected positions.

11. The device of claim 1 wherein the container holds the gaseous potentiating
15 substance at approximately 60 atmospheres and the volume of the chamber is between .07 and .33 cc.

12. The device of claim 1 wherein the valve is biased closed by a second
spring.

20

13. The device of claim 1 further including a sleeve forming an opening and positioned in the venturi region of the exit passage; said sleeve axially translatable within the exit passage and operationally connected to the valve such that movement of the valve to an open position simultaneously moves the opening to be aligned with the
25 capillary passage.

14. A method for controlling the effect of a drug on an individual comprising:
Administering the drug;
Generating a flow of a gaseous physiologically active agent; and
30 Infusing at least one facial orifice of the individual with the gaseous physiologically active agent to enhance the action of the drug.

15. A method as in claim 14, wherein the orifice is selected from the group consisting of: at least one eye, at least one ear, at least one nostril and a mouth.

35

5 16. A method as in claim 14, wherein the gaseous physiologically active agent is selected from the group consisting of carbon dioxide, nitric oxide, nitrous oxide, oxygen, helium, dilute mixtures of nitric oxide, and isocapnic mixtures of acid gases.

10 17. A method as in claim 14, wherein the orifice is selected from the group consisting of a nostril and a mouth, and wherein the individual substantially inhibits the passage of the gaseous physiologically active agent into the trachea and lungs by limiting inhalation of the gaseous physiologically active agent.

15 18. A method as in claim 14, wherein the infusing step is performed after the administering step.

 19. A method as in claim 14, wherein the infusing step is performed coincident with the administering step.

20 20. A method as in claim 14, wherein the infusing step is performed before the administering step.

 21. A method as in claim 17, wherein the infusing step is performed after the administering step.

25 22. A method as in claim 17, wherein the infusing step is performed coincident with the administering step.

30 23. A method as in claim 17, wherein the infusing step is performed before the administering step.

 24. A method as in claim 17, wherein both a nostril and a mouth are simultaneously infused.

35 25. A method as in claim 17, wherein both nostrils are simultaneously infused.

5

26. A method as in claim 18, wherein the infusing step further includes the individual inhaling the gaseous physiologically active agent.

27. A method as in claim 14 wherein the gaseous physiologically active agent is
10 carbon dioxide and the infusing step further includes the individual inhaling the carbon dioxide simultaneously with ambient air and the generating step further includes generating a flow of the carbon dioxide at a rate sufficient to produce a concentration of the carbon dioxide of between approximately 6% to 10% during inhalation.

15 28. A method as in claim 15 comprising at least one additional infusing step.

29. A method as in claim 14, wherein the gaseous physiologically active agent is diluted with air.

20 30. A method as in claim 14, further comprising the steps of:

Mixing the preselected amount of the drug and a preselected amount of the gaseous physiologically active agent to form a combination;

25 wherein the generating, administering and infusing steps occur substantially simultaneously and immediately after the mixing step; and the generating step further comprises generating a flow of the combination of the gaseous physiologically active agent and the drug.

30 31. A method as in claim 30, wherein the administering step further comprises inhaling the mixture of the gaseous physiologically active agent and the drug.

32. A method as in claim 14 wherein the gaseous physiologically active agent is a gas.

35

5 33. A method as in claim 14 wherein the gaseous physiologically active agent is a vapor.

 34. A method as in claim 14 wherein the infusing step further includes the individual inhaling the gaseous physiologically active substance simultaneously with
10 ambient air and the generating step further includes generating a flow of the gaseous physiologically active substance at a rate sufficient to produce a preselected concentration of the gaseous physiologically active substance during inhalation.

 35. A method as in claim 14 wherein the gaseous physiologically active agent is
15 carbon dioxide and the infusing step further includes the individual inhaling the carbon dioxide simultaneously with ambient air and the generating step further includes generating a flow of the carbon dioxide at a rate sufficient to produce a concentration of the carbon dioxide of between approximately 5% to 70% during inhalation.

20 36. A device for generating a controlled flow of gas from a pressurized gas container that forms an opening sealed with a cap and having a known internal pressure comprising:

 a head adapted for attachment to the container; said head forming an interior chamber and at least one outlet in communication with the interior chamber through an
25 exit passage; wherein, when the head is attached to the container, the opening is within the chamber and wherein the opening and cap are axially translatable within the chamber;

 a needle attached to the head and positioned in the chamber and adapted for perforating the cap when the opening and cap are at a preselected position in the chamber to form an orifice of a preselected diameter in the cap, and wherein the needle is
30 axially translatable; a spring engaged with the needle that holds the needle in the orifice; and a lever for actuating the needle such that operation of the lever lifts the needle from the orifice and compresses the spring, whereby gas from the pressurized container is released through the outlet.

35 37. The device of Claim 36 wherein that portion of the container near the

- 5 opening is substantially cylindrical and defines a first set of screw threads and the interior chamber includes second set of screw threads adapted for mating with the first set of screw threads.

38. The device of Claim 36 wherein the needle comprises:
10 a needle body having a penetrating tip and a proximal conical shaft with a first region near the penetrating tip and a second region removed from the penetrating tip, and wherein the orifice is formed by the penetrating tip and enlarged to a selected diameter by the second region of the conical shaft; and
wherein the first region of the conical shaft defines a taper angle of greater than
15 25° and the second region of the conical shaft defines a taper angle of between 2° and 6°.

39. The device of claim 36 wherein the exit passage further includes a venturi region and the head further forms an air inlet passage communicating between the ambient atmosphere and the venturi region.

20

40. A dispenser as in claim 36 wherein the diameter of the orifice is selected to provide a maximum flow of between approximately 100 and 400 cc/sec of gas.

41. A flow regulator, adapted for attachment to a container of pressurized gas
25 that forms an opening sealed with a cap, for providing a flow of therapeutic gas to a individual comprising:

a head, a tubular sleeve having a first end and a second end, and a tubular collar; wherein

- the collar is adapted for fixed attachment to the container adjacent to and
30 surrounding the opening and cap and defines a first set of external screw threads;

the head defines a first and second end with an outlet at the first end and an exit passage between the outlet and the second end of the head, and wherein the second end of the head is adapted to be placed adjacent to the cap and defines a second set of external screw threads;

- 35 the head and collar are connected to allow axial translation of the head relative to

5 the collar and container and to prevent rotational movement of the head relative to the collar and container; and

the tubular sleeve defines a third set of screw threads at the first end adapted to mate with the first set of screw threads and a fourth set of screw threads at the second end adapted to mate with the second set of screw threads; and wherein the first and third sets
10 of screw threads are slightly coarser than the second and fourth sets of screw threads and the head further includes:

a needle fixed to and extending from the second end of the head, said needle adapted for perforation of the cap when the cap and the second end of the head are at a preselected distance from each other and further adapted to form and seal an orifice of
15 selected size at preselected distances of cap penetration, such that partial removal of the needle permits a flow of gas from the orifice in an amount related to the distance the needle is removed;

whereby when the screw threads are mated, the flow regulator is attached to the container and the orifice is formed by the needle, the amount of gas flow from the outlet
20 may be selected by rotating the sleeve to effect the axial translation of the head and needle.

42. A flow regulator as in claim 41 wherein the head further includes a detent, whereby the rotation of the sleeve and the axial translation of the head and needle may be
25 adjusted to preselected positions.

43. A flow regulator as in claim 41 wherein the sleeve and collar include indicator markings.

30 44. A flow regulator as in claim 41 wherein the collar includes indicator markings for showing the relative position of the collar and the container whereby the amount of maximum needle penetration, the orifice size and the maximum flow rate are indicated; and the sleeve includes indicator markings for showing the relative position of the sleeve and the collar whereby the distance the needle has been removed from the
35 orifice and the percentage of maximum flow rate may be determined.

5

45. A flow regulator as in claim 42 wherein the collar includes indicator markings for showing the relative position of the collar and the container whereby the amount of maximum needle penetration, the orifice size and the maximum flow rate are indicated; and the sleeve includes indicator markings for showing the relative position of the sleeve and the collar whereby the distance the needle has been removed from the orifice and the percentage of maximum flow rate may be determined.

15

46. The method of claim 14 wherein the gaseous physiologically active agent is vasoactive.

47. The method of claim 14 wherein the gaseous physiologically active agent is neuroactive.

48. The method of claim 14 wherein the gaseous physiologically active agent is myoactive.

20

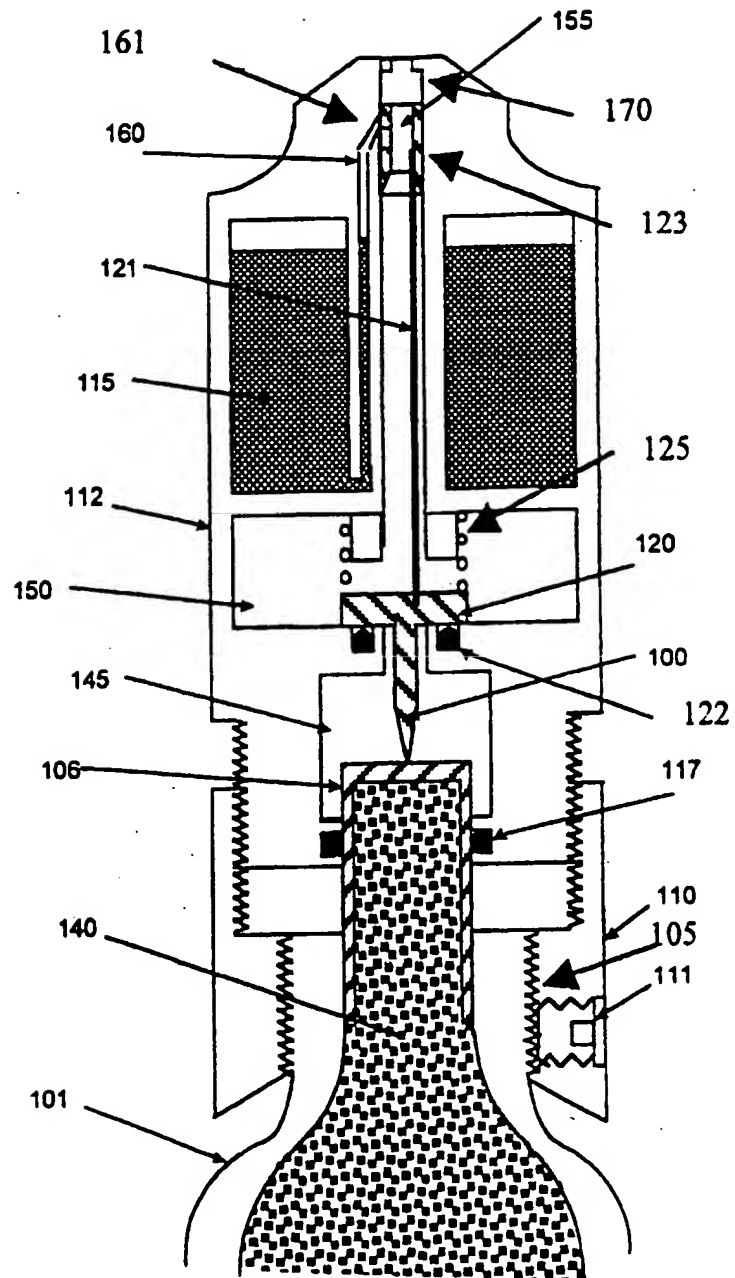


Fig. 1

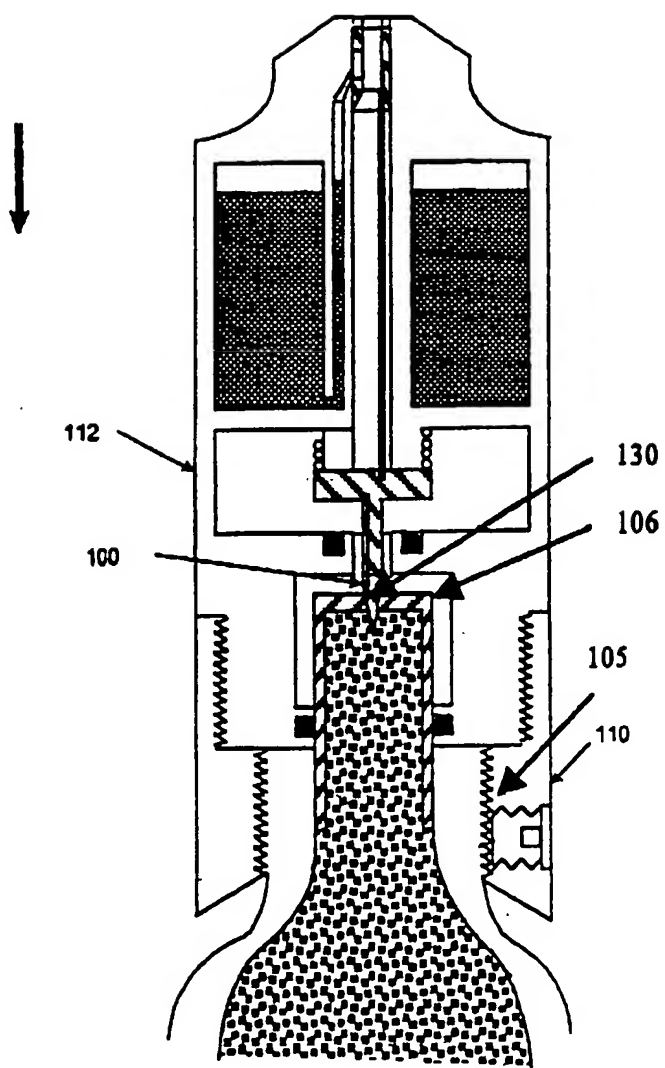


Fig. 2

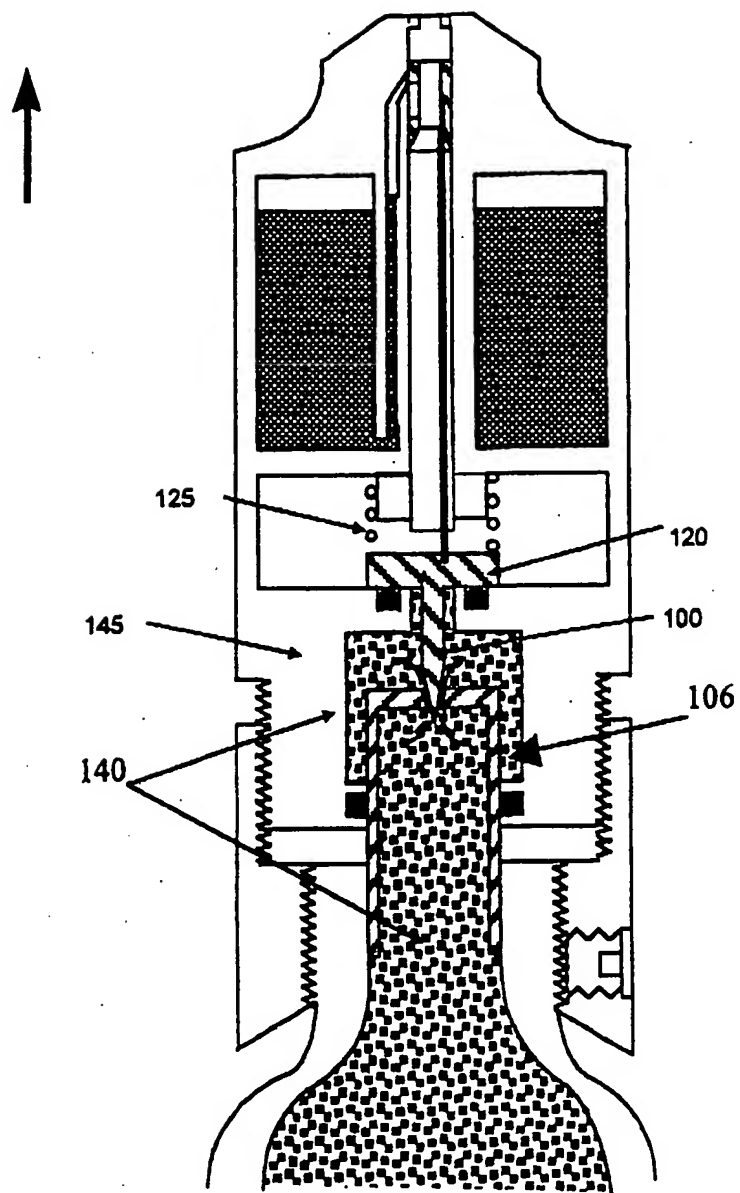


Fig. 3

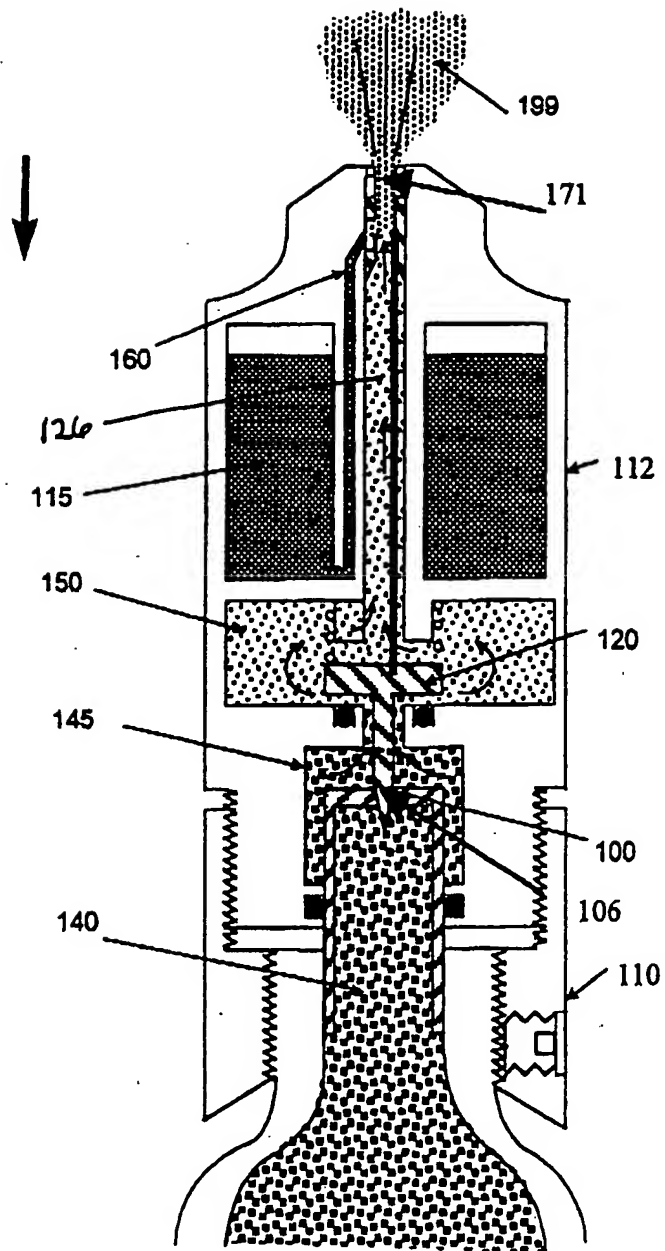


Fig. 4

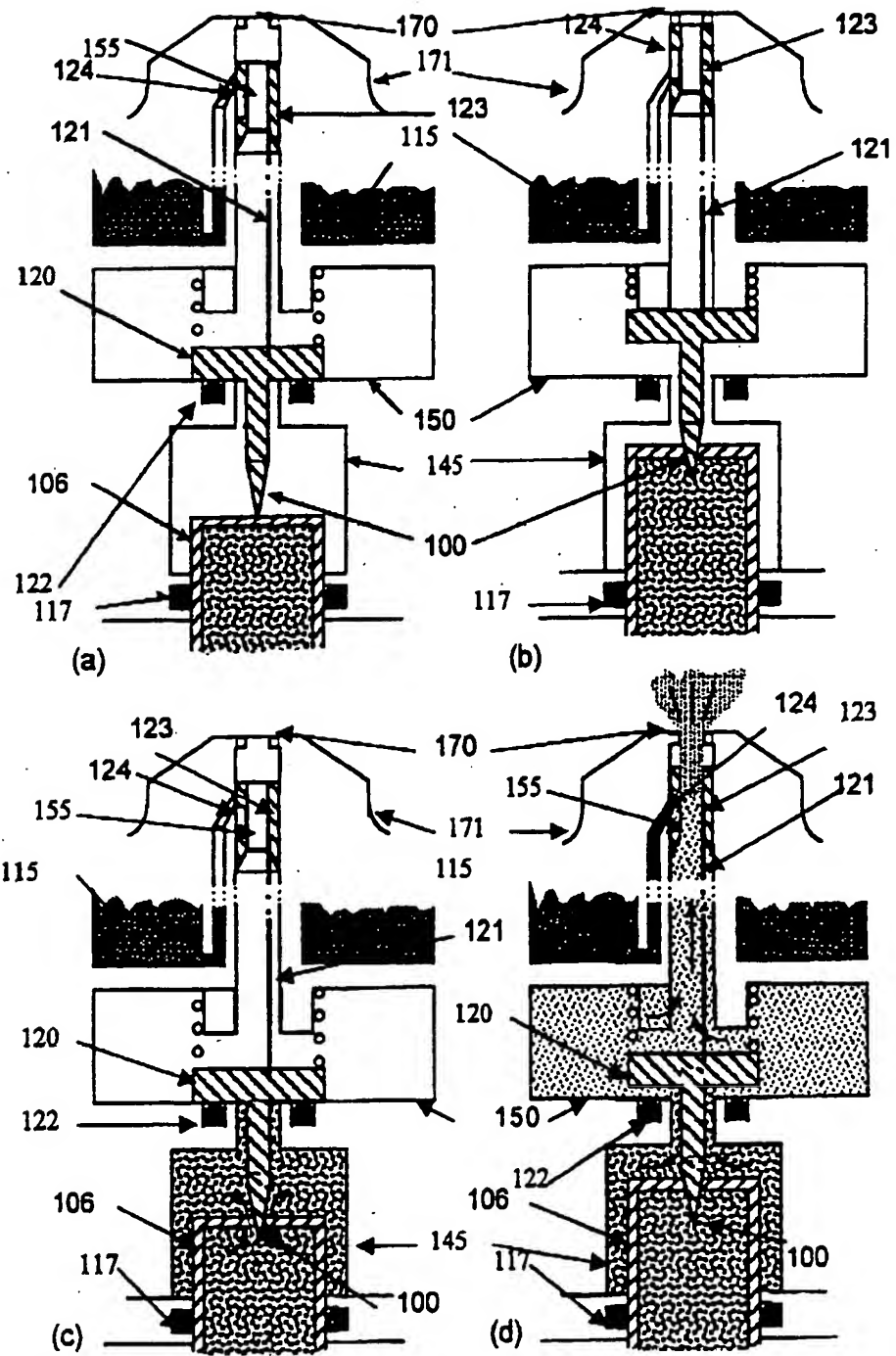


Fig. 5

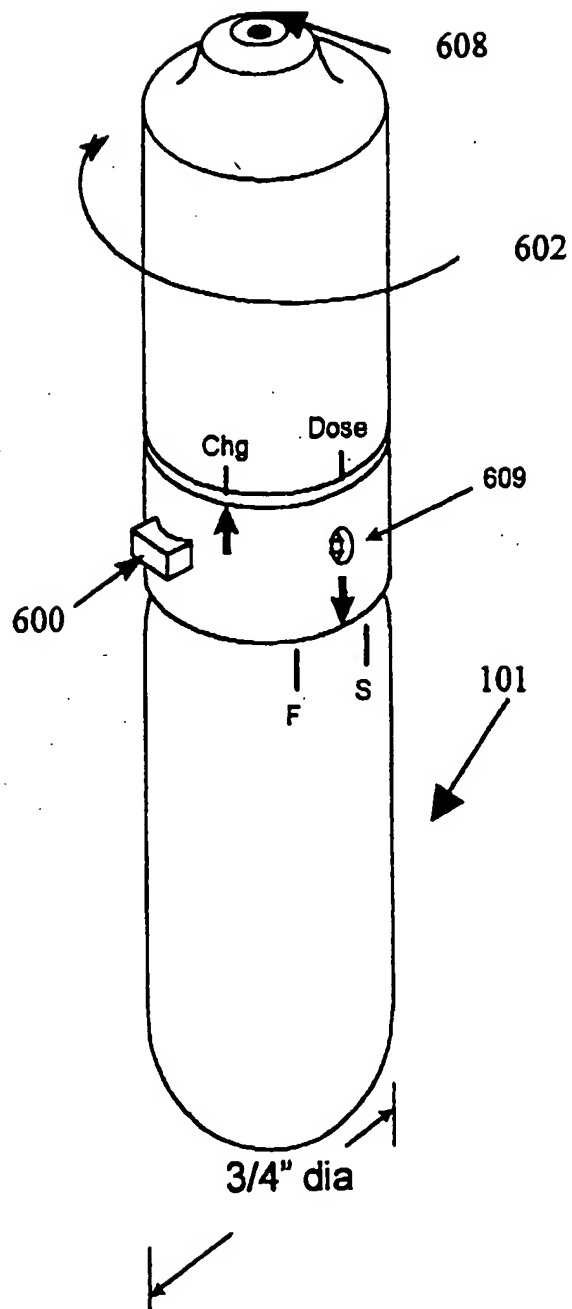


Fig. 6

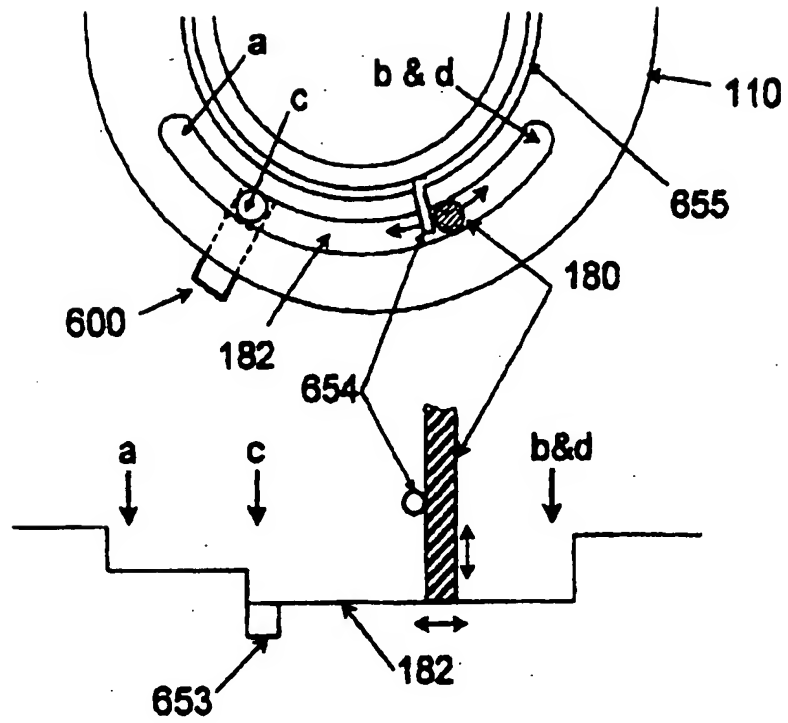


Fig. 7

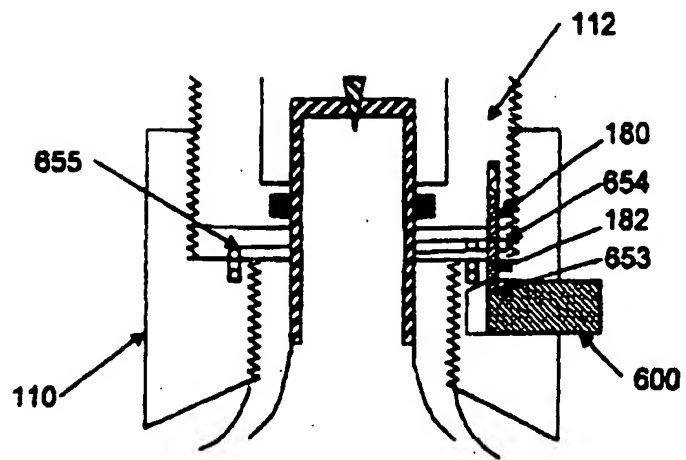


Fig. 7a

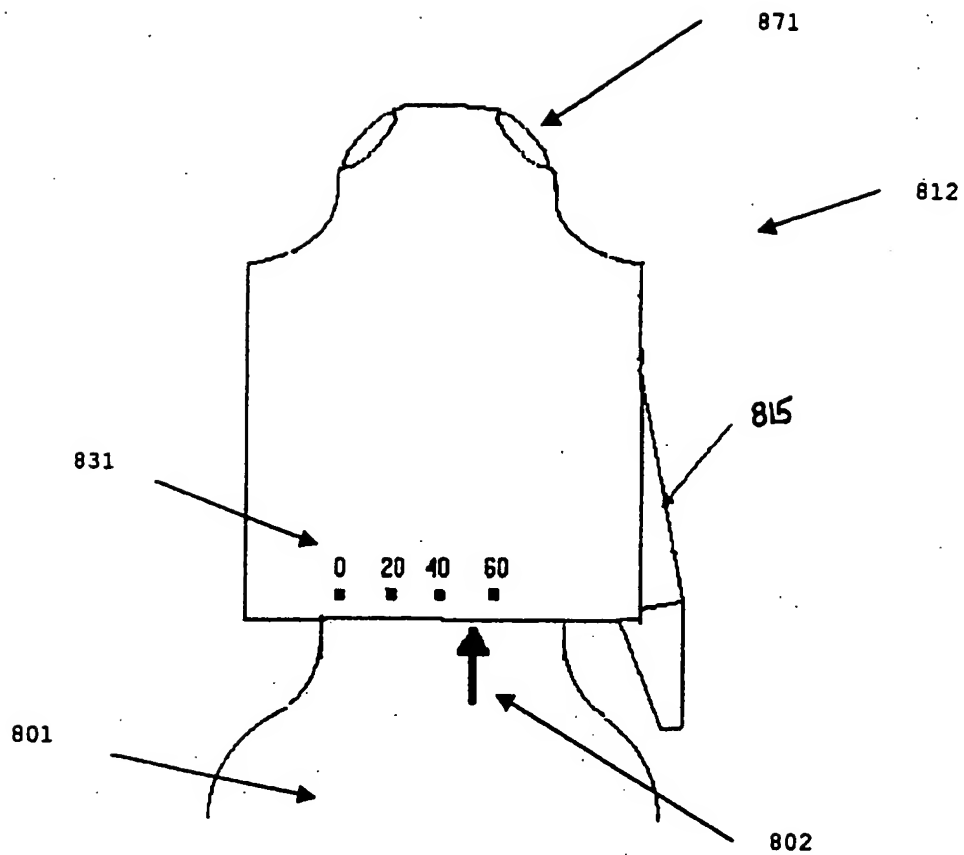


Fig. 8a

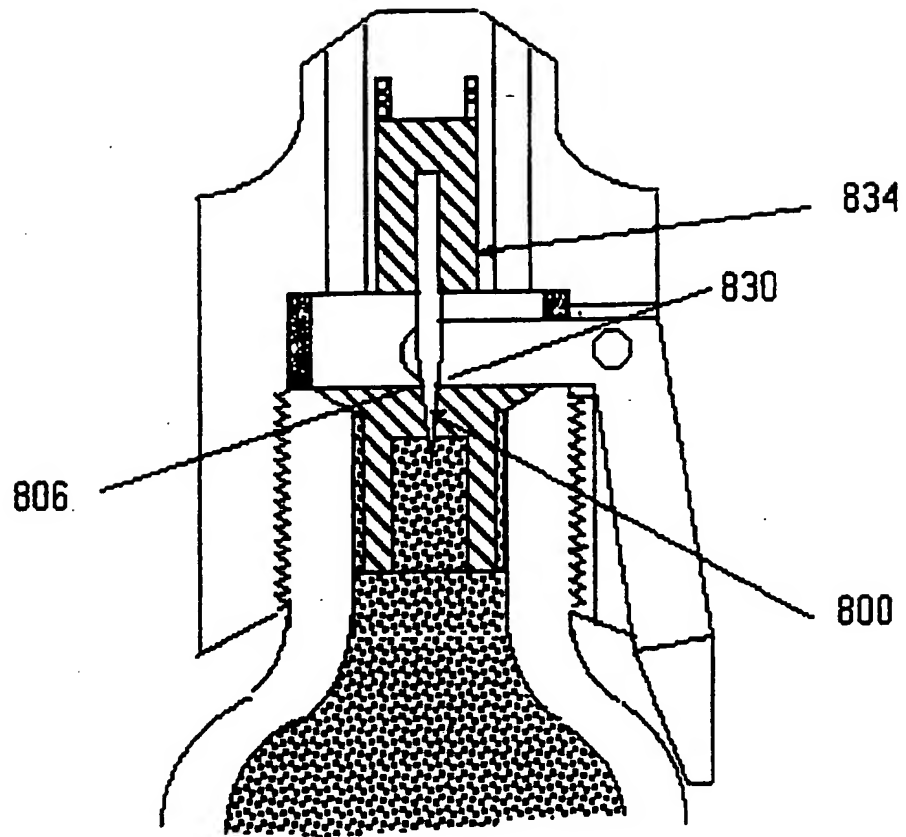


Fig. 9

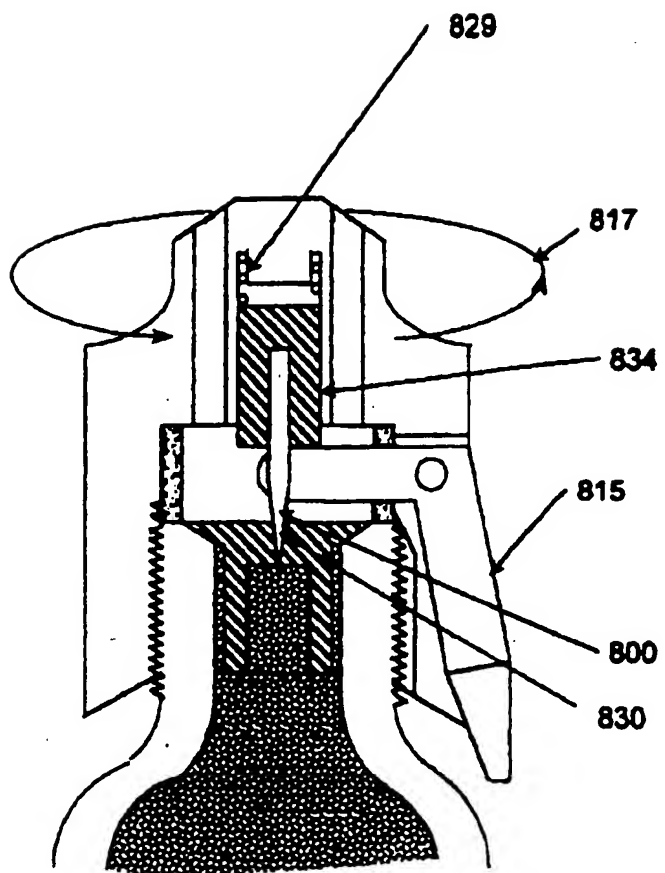


Fig. 10

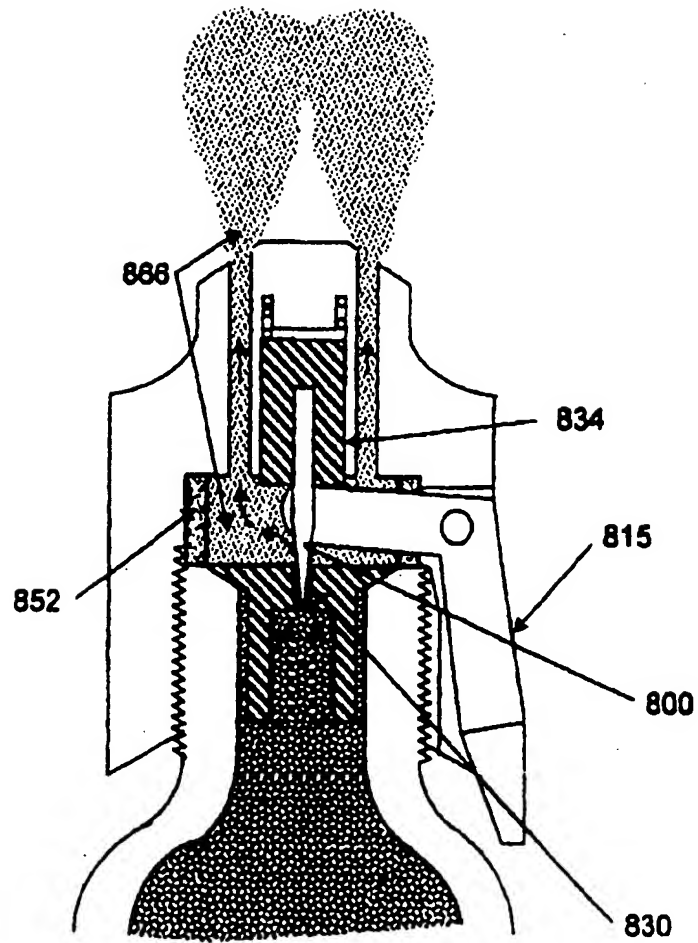


Fig. 11



Fig 12A

P



Fig. 12B

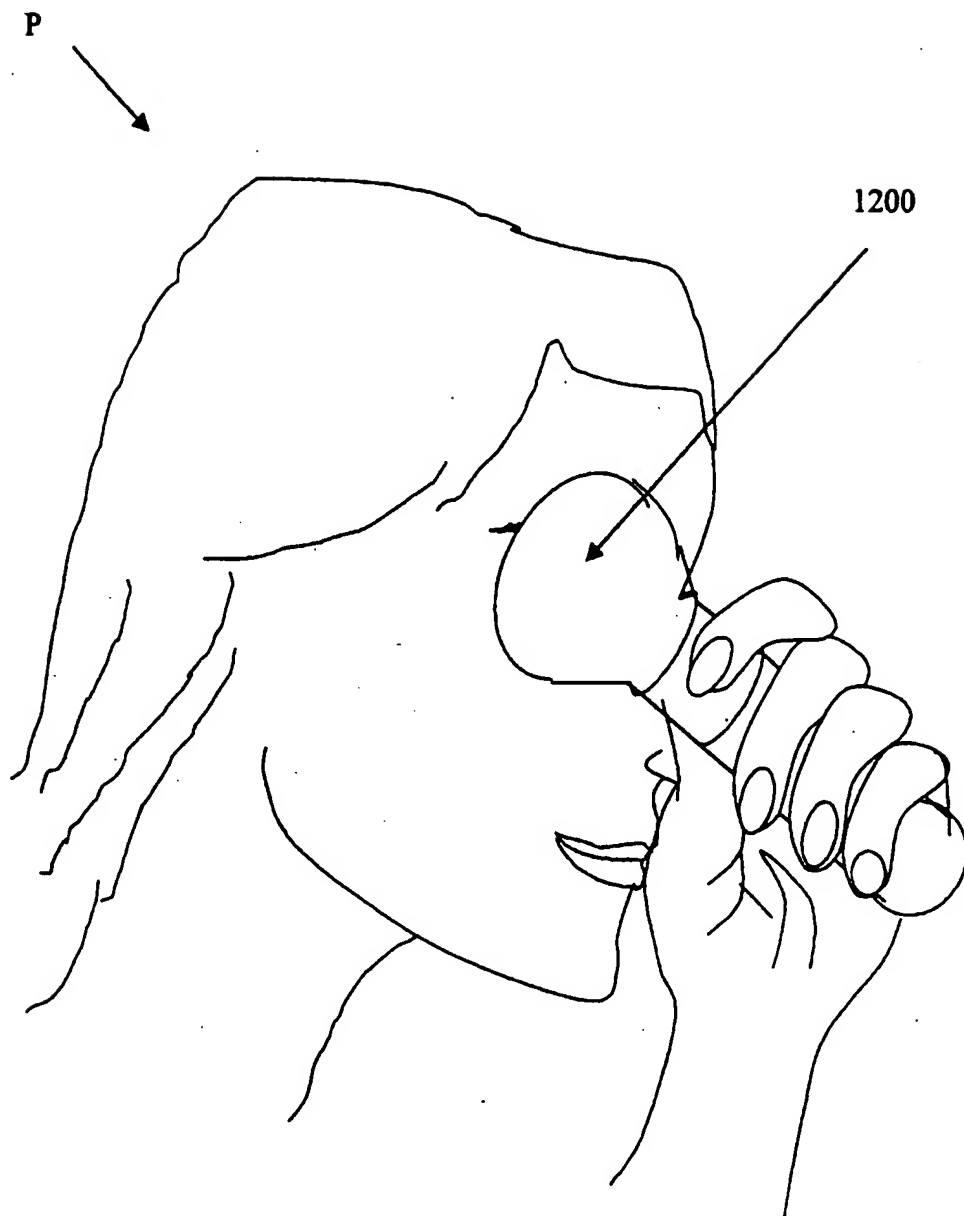


Fig. 12C



Fig. 12D

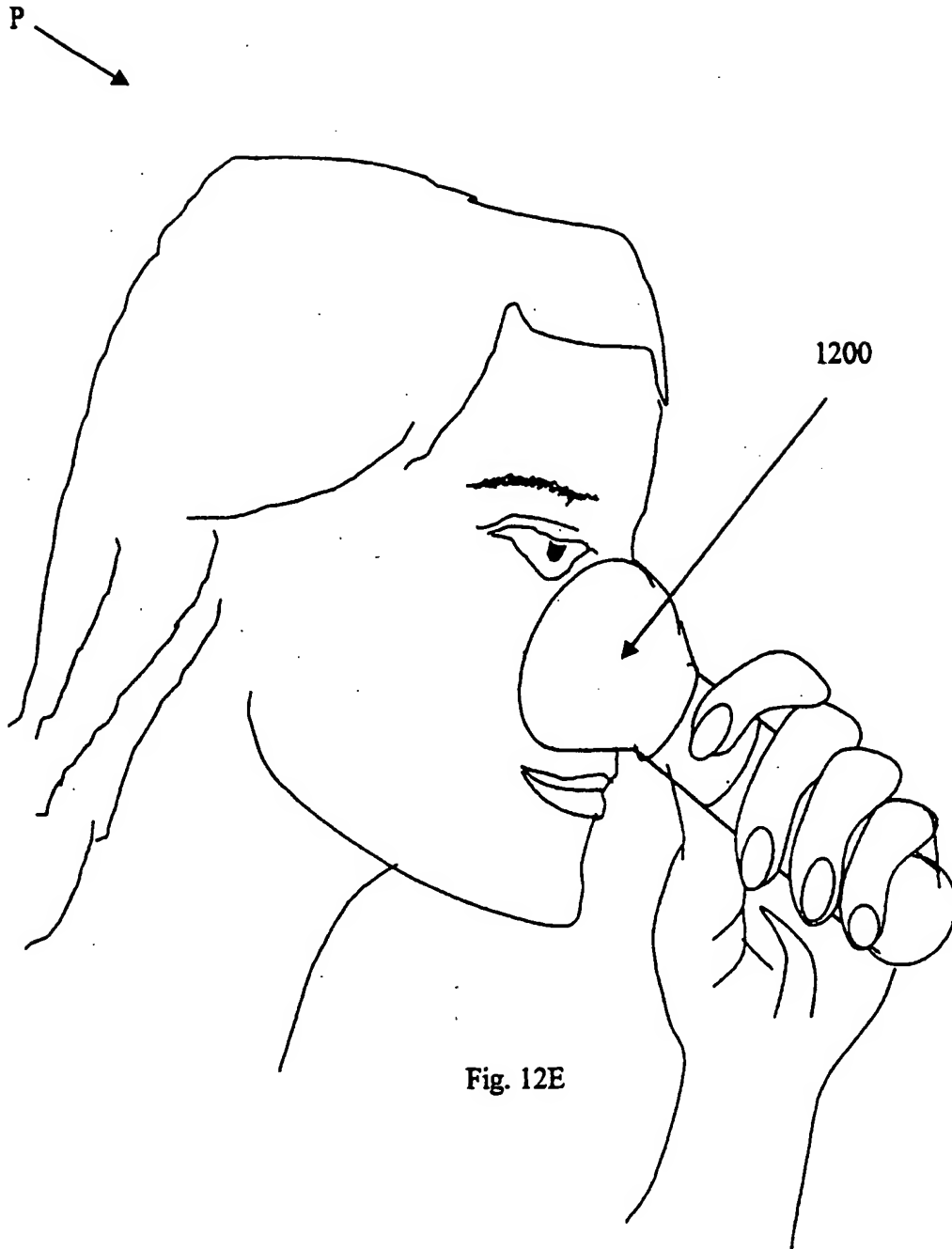


Fig. 12E

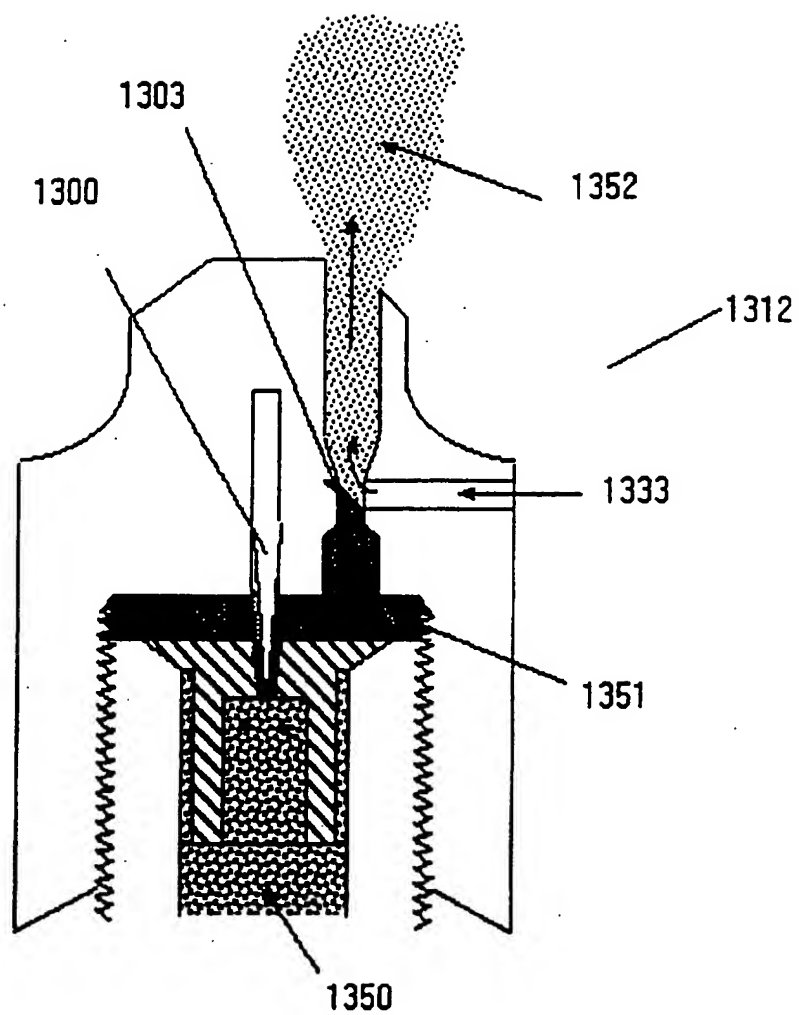
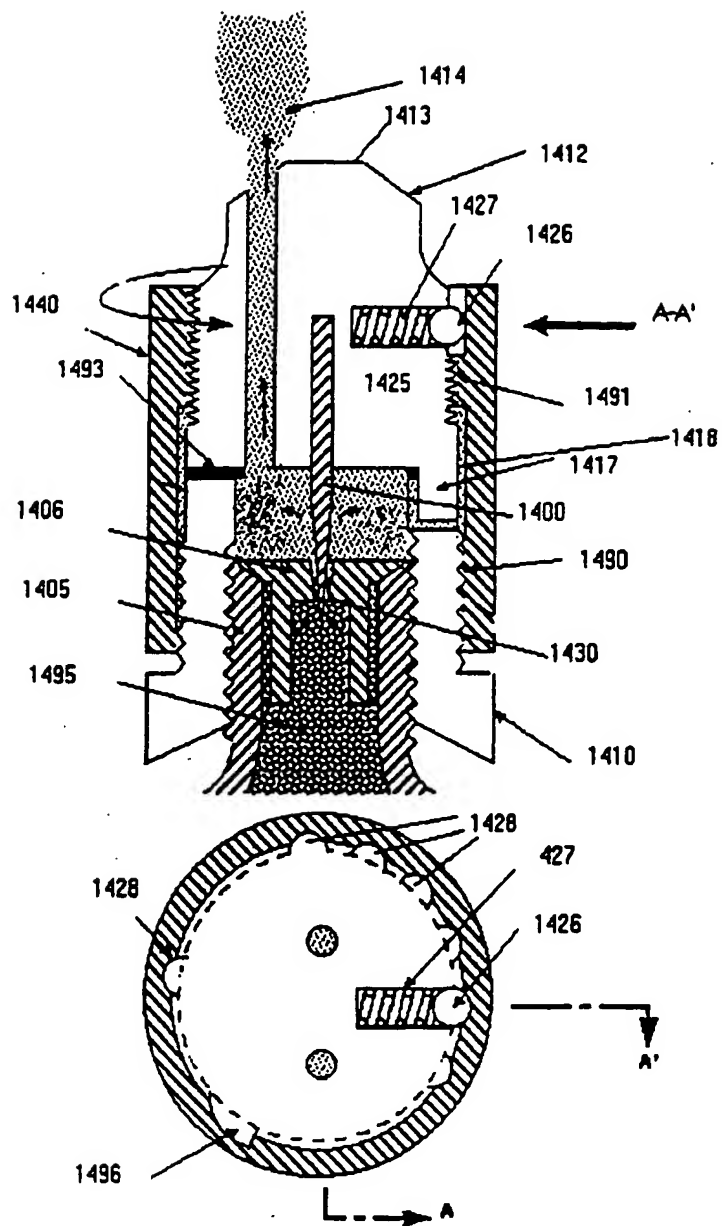
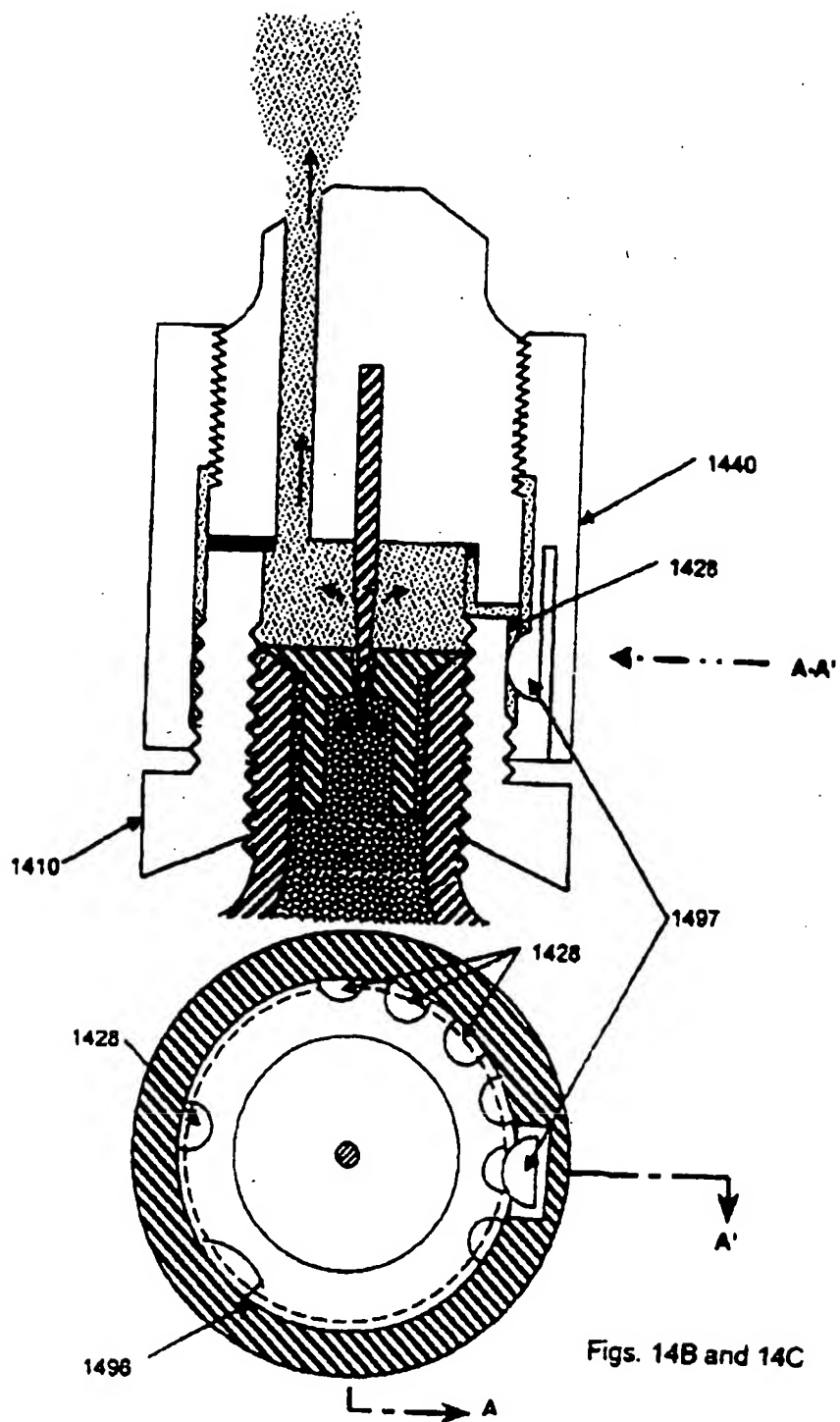


Fig. 13



Figs 14 and 14A



Figs. 14B and 14C

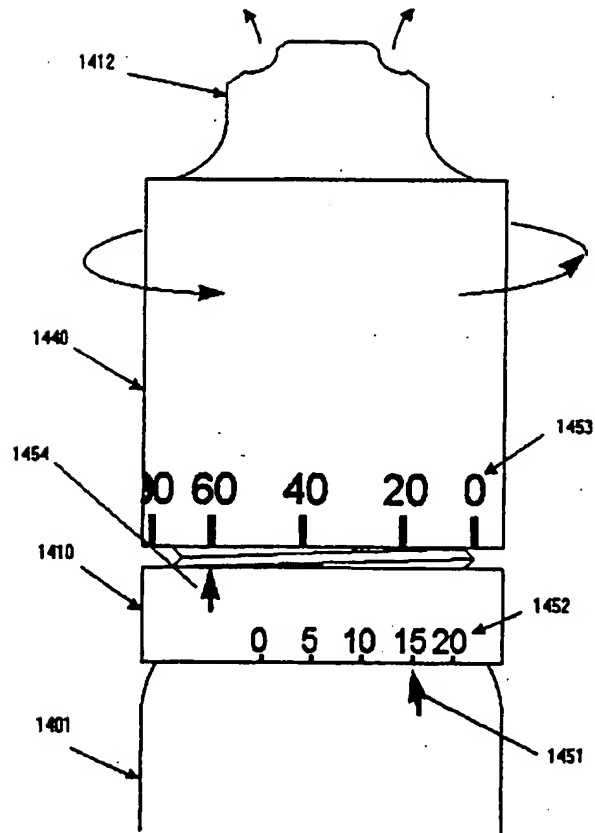


Fig. 15

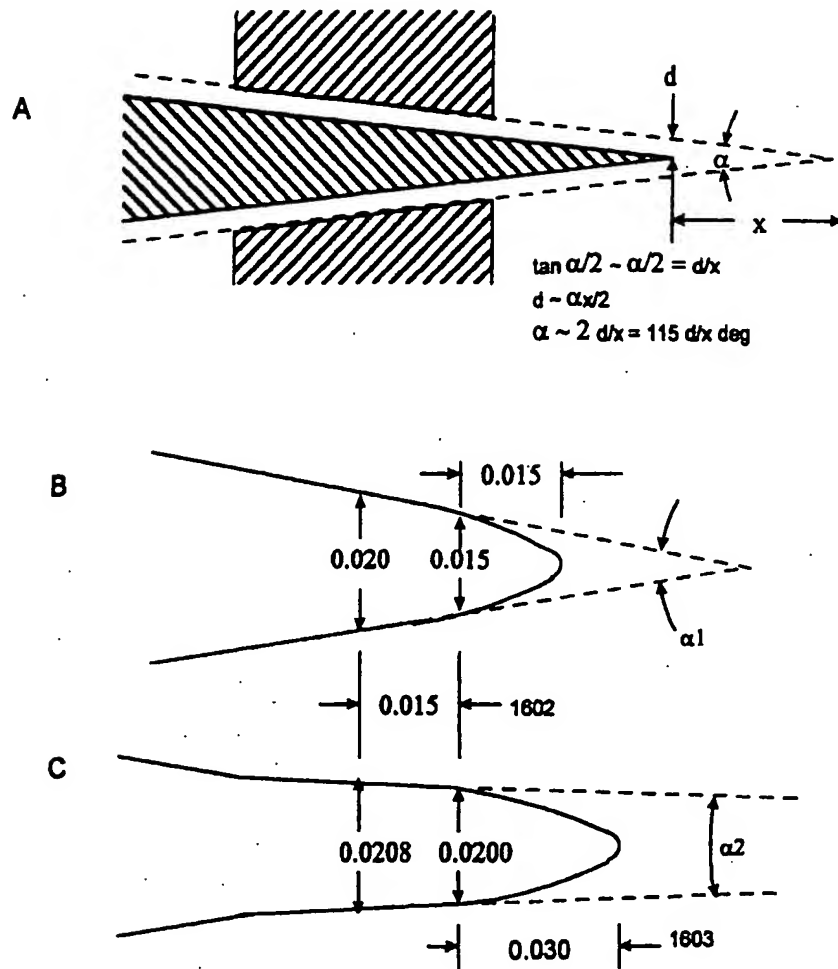


Fig. 16